

**MOS in saturazione**

$$G \triangleq \frac{v_{out}}{v_{in}} = -g_m R_D$$

- aumentare  $g_m$

$$g_m = 2k_n (V_{GS} - V_{Th}) = 2 \left( \frac{1}{2} \mu_n C_{ox} \frac{W}{L} \right) (V_{GS} - V_{Th})$$

• aumentare  $R_D$

$$I_D = k_n (V_{GS} - V_{Th})^2 (1 + \lambda V_{DS})$$

$$\lambda = \frac{1}{|V_A|}$$

↑ effetto di moduloz dell'az funziozz di conat

$$r_o = \left[ \frac{\partial I_D}{\partial V_{DS}} \right]_{sat}^{-1} = \frac{|V_A|}{I_D}$$

$$r_o \approx 50k\Omega \div 100k\Omega$$

$$G \triangleq \frac{v_{out}}{v_{in}} = -g_m (R_D \parallel r_o)$$

↑ ↑ ↑

↑ ↑ ↑

**STADIO SOURCE A MASSA CON CARICO ATTIVO**

- in assenza di  $r_o$

$$v_{out} = -g_m v_{in} r_{out} \Rightarrow G = -g_m r_{out}$$

- tenendo conto di  $r_o$

$$v_{out} = -g_m v_{in} (r_{out} \parallel r_o)$$

$$\hookrightarrow G = -g_m (r_{out} \parallel r_o)$$

**GEN. DI CORRENTE A MOSFET**

**STADIO SOURCE DEGENERATO CON CARICO ATTIVO**

$$I = |k_p| (V_{GS} - V_{Th})^2$$

trascurando  $r_{o1}$

Intervallo di tensioni possibili per il modo  $v_{out}$

- $V_{GS2} > V_{Th}$
- $V_{GS1} < V_{Th}$
- $V_{GS2} - v_{out} > V_{Th}$
- $V_{GS1} - v_{out} < V_{Th}$
- $v_{out} < V_{GS2} - V_{Th}$
- $v_{out} > V_{GS1} - V_{Th}$

$(V_{GS1} - V_{Th}) < v_{out} < (V_{GS2} - V_{Th})$

su segnale

$$i_D = g_m v_{gs}$$

$$v_{gs} = \frac{v_{in}}{\frac{1}{g_m} + R_S}$$

$$v_{out} = -i_D r_{o2} = -\frac{r_{o2}}{\frac{1}{g_m} + R_S} v_{in}$$

$$\hookrightarrow G \triangleq \frac{v_{out}}{v_{in}} = -\frac{r_{o2}}{\frac{1}{g_m} + R_S} = -\frac{g_m r_{o2}}{1 + g_m R_S}$$

$G_{HF} \triangleq -g_m r_{o2}$

Circuito in HF tenendo conto di entrambe le  $r_o$

su segnale

$$v_{out} = -g_m v_{gs} (r_{o1} \parallel r_{o2})$$

**GEN. DI CORRENTE CON MOSFET CON DEGENERAZIONE DI SOURCE**

- \* in assenza di  $r_o$

$$R_{out} = \infty$$

$$R_{out} \triangleq \frac{v_p}{i_p}$$

Circuito di piccolo segnale polarizzato in saturazione

$$i_p = g_m v_{gs} + i_{r_o}$$

$$v_{gs} = i_p R_S \Rightarrow v_{gs} = -i_p R_S$$

$$i_{r_o} = \frac{v_p - v_{gs}}{r_o}$$

$$i_p = -i_p g_m R_S + \frac{v_p}{r_o} - i_p \frac{R_S}{r_o}$$

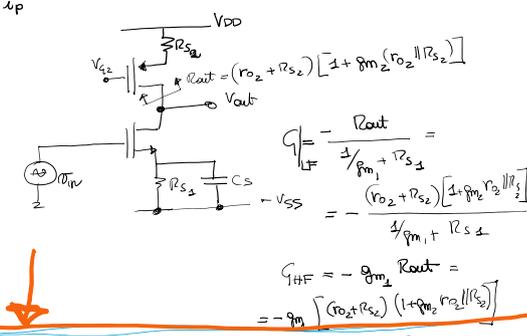
$$i_p \left[ 1 + g_m R_S + \frac{R_S}{r_o} \right] = \frac{v_p}{r_o}$$

$$A_p = -A_p g_m R_s + \frac{V_p}{r_o} - r_o$$

$$A_p \left[ 1 + g_m R_s + \frac{R_s}{r_o} \right] = \frac{V_p}{r_o}$$

$$V_p = r_o \left[ 1 + g_m R_s + \frac{R_s}{r_o} \right] A_p$$

$$R_{out} \triangleq \frac{V_p}{A_p} = r_o + R_s + g_m R_s r_o = (r_o + R_s) \left[ 1 + g_m r_o R_s \right]$$

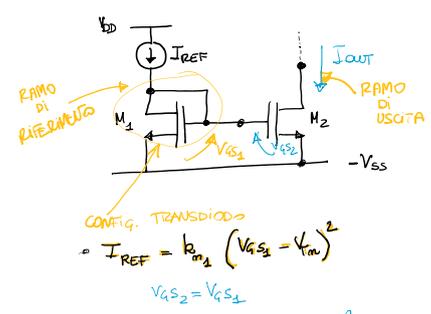


$$G_{LF} = \frac{R_{out}}{\frac{1}{g_{m1}} + R_{s1}} = \frac{(r_{o2} + R_{s2}) [1 + g_{m2} r_{o2} R_{s2}]}{\frac{1}{g_{m1}} + R_{s1}}$$

$$G_{HF} = -g_{m1} R_{out} = -g_{m1} (r_{o2} + R_{s2}) (1 + g_{m2} r_{o2} R_{s2})$$

# FINE ARGOMENTI PRIMA PROVA IN ITINERE

## SPECCHIO DI CORRENTE (CURRENT MIRROR)



$$I_{out} = k_{m2} I_{REF} = \frac{\frac{1}{2} \mu_n C_{ox} (W/L)_2}{\frac{1}{2} \mu_n C_{ox} (W/L)_1} I_{REF} = \frac{(W/L)_2}{(W/L)_1} I_{REF}$$

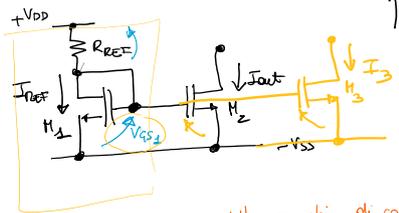
CONFIG. TRANSDIODO

$$I_{REF} = k_{m1} (V_{GS1} - V_{th})^2$$

$$V_{GS2} = V_{GS1}$$

$$I_{out} = k_{m2} (V_{GS2} - V_{th})^2 = k_{m2} (V_{GS1} - V_{th})^2 = \frac{I_{REF}}{k_{m1}} k_{m2}$$

a patto che ciò che è connesso al drain di M2 lo mantenga asturo

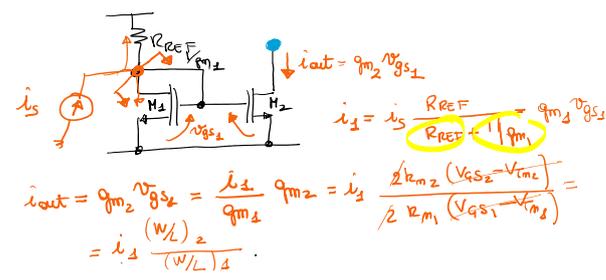


$$I_{REF} = k_{m1} (V_{GS1} - V_{th})^2$$

$$\left[ V_{DD} - (-V_{SS}) \right] = I_{REF} R_{REF} + V_{GS1}$$

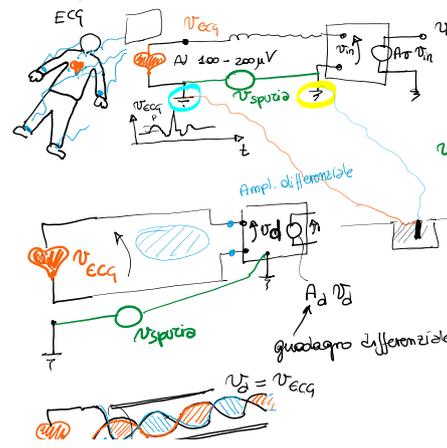
(V\_GS1, I\_REF)

Completamento dello specchio di corrente su piccolo segnale



$$i_{out} = g_{m2} v_{gs2} = \frac{i_s}{g_{m1}} g_{m2} = i_s \frac{\frac{1}{2} k_{m2} (V_{GS2} - V_{th})^2}{\frac{1}{2} k_{m1} (V_{GS1} - V_{th})^2} = i_s \frac{(W/L)_2}{(W/L)_1}$$

## STADIO DIFFERENZIALE



$$v_{out} = A_v v_{in} = A_v v_{ECG} = 1000 \times 100 \mu V = 100 mV$$

$$v_{out} = A_v v_{in} = A_v (v_{ECG} + v_{spurio}) = 1000 V \cdot 1 \mu V = 1 V$$

